

# Non-linear Structural Analysis Technique Based on Flexibility Method by Pade Approximants, Application on Spherical Assemblies

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# Outlines

- 1. Introduction
- 2. Geometrical nonlinear force method
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#### 1. Introduction

•Spheres are always considered unique and elegant geometry for structures.

•Due to the geometrical characteristics of spheres, they are used to afford a wide span as a lightweight structure with economical choice.



Fig. 1. Al Wasl plaza spherical structure

#### 1. Introduction

•When they are affected by specific external loads, they face notable deformation.

•Precise computation during the analysis and design process considering their geometrical

nonlinear behavior.

•Analysis approaches:

✓ Dynamic relaxation, ✓ Minimum potential energy, ✓ Finite element, ✓ Force method.

#### 1. Introduction

•An alternative approach is conducted in analyzing the spherical model which is a nonlinear geometrical structure.

•The proposed technique is based on the nonlinear force method expanded using the Pade approximation method.



(3)



Fig. 2. (a) Original and deformed length of element 1-2. (b) Original and deformed equilibrium state of element 1-2.

Where:

Q(d): equilibrium matrix at the deformed configuration.

*t*: internal force.

**P:** external force.

C(d): the compatibility matrix at the deformed configuration.

d: nonlinear nodal displacement.

 $e_o(d)$ : nonlinear member actuation. F: flexibility matrix  $F = \frac{L_o}{AE}$ 

$$e = L_{c} - L_{o}$$

$$L_{c} = \left\{ \left( x_{ji} + dx_{ji} \right)^{2} + \left( y_{ji} + dy_{ji} \right)^{2} + \left( z_{ji} + dz_{ji} \right)^{2} \right\}^{\frac{1}{2}}$$

$$L_{c} = \left( L_{o}^{2} + 2x_{ji}dx_{ji} + 2y_{ji}dy_{ji} + 2z_{ji}dz_{ji} + dx_{ji}^{2} + dy_{ji}^{2} + dz_{ji}^{2} \right)^{\frac{1}{2}}$$

 $\left|L_{o}^{2}\right\rangle$ 

 $/I^{2}$ 

 $L_c = \left(L_o^2 + H\right)^{\frac{1}{2}}$ 

L

$$L_{c} = L_{o} \left( 1 + H/L_{o}^{2} \right)^{\frac{1}{2}} \qquad L_{c} = L_{o} \left( \frac{4 + 3H}{4 + H/L_{o}^{2}} \right)^{\frac{1}{2}}$$



$$e = L_{o} \times \left\{ \begin{pmatrix} 4 + \frac{3\left(2x_{o}dx_{o} + 2y_{o}dy_{o} + dx_{ji}^{2} + dy_{ji}^{2}\right)}{L_{o}^{2}} \\ \frac{4}{4} + \frac{\left(2x_{o}dx_{o} + 2y_{o}dy_{o} + dx_{o}^{2} + dy_{o}^{2}\right)}{L_{o}^{2}} \end{pmatrix} - 1 \right\}$$
(4)  
$$P_{x} = \pm t \times \cos \theta \\ P_{y} = \pm t \times \sin \theta$$
(5)



$$\cos\theta = \frac{x_o + dx_o}{L_o + e} = \frac{4x_oL^2 + 4dx_oL^2 + 2x_o^2dx_o + 2x_oy_ody_o}{4L^3 + 6L(x_odx_o + y_ody_o)}; \quad \sin\theta = \frac{y_o + dy_o}{L_o + e} = \frac{4y_oL^2 + 4dy_oL^2 + 2y_o^2dy_o + 2y_ox_odx_o}{4L^3 + 6L(x_odx_o + y_ody_o)};$$

#### 3. Numerical example





Fig. 4. Laterally loaded in (N) spherical model

Fig. 3. Double-layer spherical model



SND

#### 4. Result

Node numbers

Fig. 5. Differences of resultant displacement obtained through nonlinear and linear force methods with respect to SAP2000

#### 4. Result



Fig. 6. Difference of maximum compressive and tensile member forces of SNF and SLF

# 5. Conclusion

- 1) The newly derived nonlinear geometrical analysis force method is proposed and applied to the double-layer spherical structure.
- 2) The analysis result was validated using the nonlinear finite element software SAP2000.
- 3) The maximum discrepancy for both the displacement and member force between nonlinear analysis results were 0.2% and 0.1% respectively.
- 4) Discrepancy came out as 14.6% for displacement differences, and 17.5% and 18.6% for tensile and compressive force differences in comparison to the linear approach.

# 5. Conclusion

- 5) The results showed the applicability of the technique in analyzing such a complex structure by concerning the nonlinear behavior of the structures.
- 6) The employment of the Pade approximation method in expanding the nonlinear member variation and internal force components provided a very convergeable function in solving the nonlinear equations.

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